



Uncertainty-based multidisciplinary design optimization of lunar CubeSat missions

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Outline

Uncertainty-based multidisciplinary design optimization of lunar CubeSat missions



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Optimization Methodology

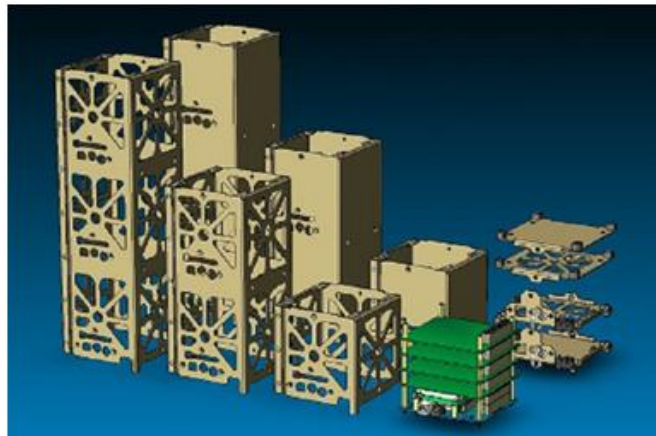
Results & Discussions

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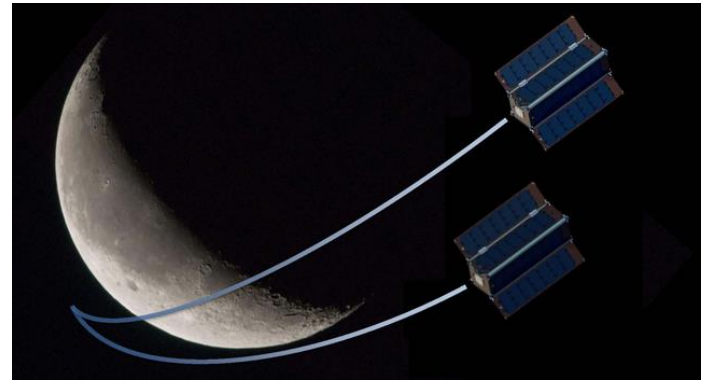
Introduction

Uncertainty-based multidisciplinary design optimization of lunar CubeSat missions

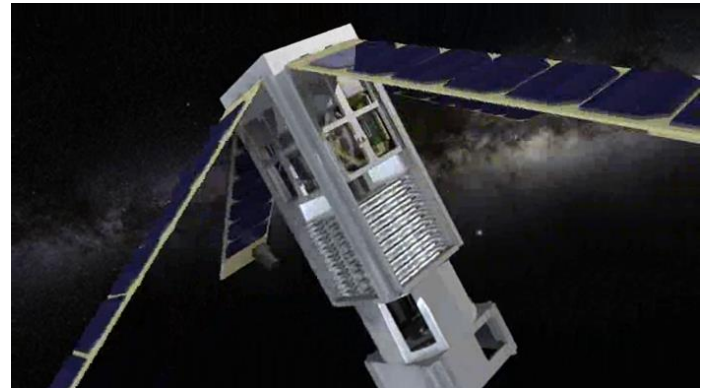
- Cost-effective shift
 - Large-scale to small-scale
 - Successful heritage, easy launch, much lower cost, faster development



3U, 2U, 1U cubic cells



Dual INSPIRE CubeSats by NASA

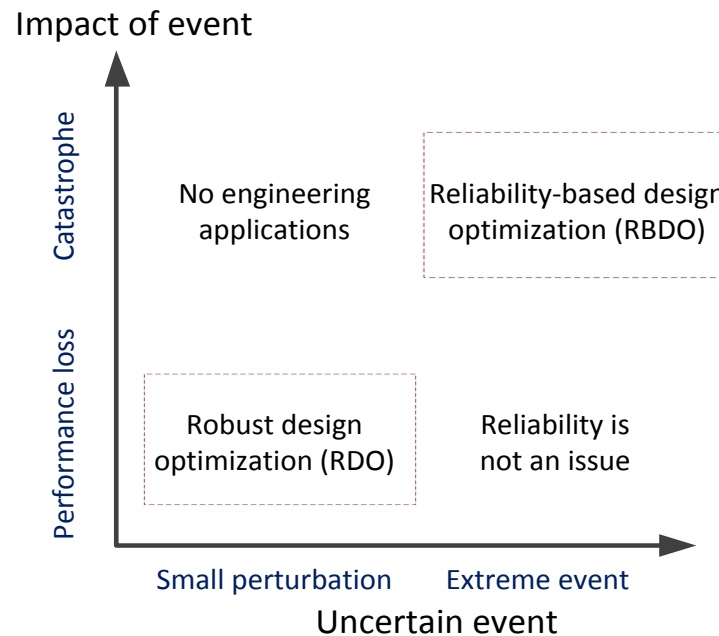


3U CubeSat by PocketSpacecraft

Introduction

Uncertainty-based multidisciplinary design optimization of lunar CubeSat missions

- Goals of our research
 - Multidisciplinary design optimization (MDO) under uncertainty
 - Uncertainty quantification and probabilistic optimization for lunar CubeSats
 - Cost risk minimization with regard to robustness and reliability



Problem Formulation

Uncertainty-based multidisciplinary design optimization of lunar CubeSat missions

$$\tilde{f} \approx f(s, \omega)$$

Surrogate model

Design variables

Uncertainty

The diagram illustrates the mathematical formulation of a surrogate model. The central equation is $\tilde{f} \approx f(s, \omega)$. Three blue arrows point from descriptive labels to parts of the equation: one from 'Surrogate model' to \tilde{f} , one from 'Design variables' to s , and one from 'Uncertainty' to ω . The text 'Design variables' is highlighted in red.

Problem Formulation

Uncertainty-based multidisciplinary design optimization of lunar CubeSat missions

- Lunar trajectory and orbit design
 - Edelbaum's analysis

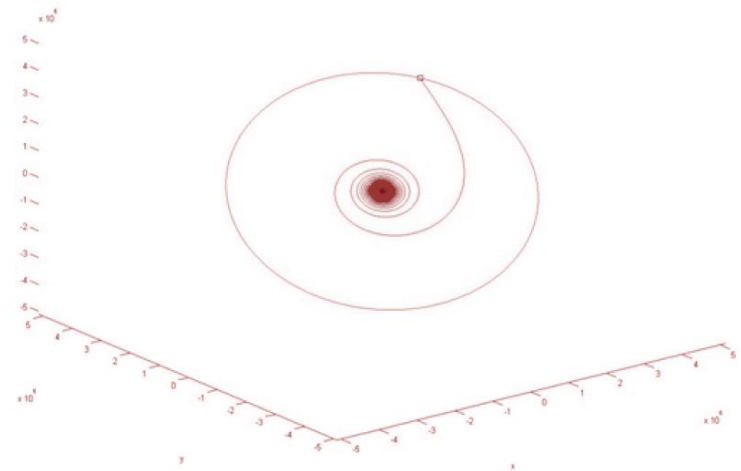
$$\Delta V = V_0 \cos \beta_0 - \frac{V_0 \sin \beta_0}{\tan\left(\frac{\pi}{2} \Delta i + \beta_0\right)}$$

$$\beta(t) = \tan^{-1}\left(\frac{V_0 \sin \beta_0}{V_0 \cos \beta_0 - a_T t}\right)$$

$$V(t) = \sqrt{V_0^2 - 2V_0 a_T t \cos \beta_0 + a_T^2 t^2}$$

$$\Delta i(t) = \frac{2}{\pi} \left[\tan^{-1}\left(\frac{a_T t - V_0 \cos \beta_0}{V_0 \sin \beta_0}\right) + \frac{\pi}{2} - \beta_0 \right]$$

$$m_p = m_{total} (1 - e^{-\Delta V / g I_{sp}})$$



Simulated spiral trajectory

Problem Formulation

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● Subsystem definition

- Propulsion: Miniature Xenon Ion (MiXI)

Engine	Thrust (mN)	Mass (kg)	Isp (s)	Power (W)	Efficiency (%)
MiXI	0.5-3	0.2	3000	13-50	~50

Source: <http://dst.jpl.nasa.gov/thrusters/>

- Key payload: CCD camera

$$D_r = \theta_x V_N \frac{h s b_{it}}{d_s^2 q} \quad d_s = \mu_0 h / f_c$$

$$S_w = 2R_e \left\{ \sin^{-1}[\sin \omega_x (h + R_e) / R_e] - \omega_x \right\} / \sin i$$

- Thermal: passive control $\sum Q_{in} - \sum Q_{out} = 0$

$$T_{sc} = \left\{ \frac{\alpha I_s [A_s F_s \cos(\theta_s) + \rho_A A_A F_A] + Q_{int} + \sigma(\varepsilon_{sp} A_{sp} + \varepsilon_R A_R) F_{sp} T_{sp}^4 + \sigma \varepsilon_{IR,sc} \varepsilon_{IR} A_{IR} F_{IR} T_{IR}^4}{\sigma(\varepsilon_{sp} A_{sp} + \varepsilon_R A_R) F_{sp} + \sigma \varepsilon_{IR,sc} \varepsilon_{IR} A_{IR} F_{IR}} \right\}$$



Problem Formulation

Uncertainty-based multidisciplinary design optimization of lunar CubeSat missions

- Uncertainty definition

Discipline	Parameter	Notation	Distribution
Orbit	Orbit altitude (km)	h	Truncated Nor.
	Lunar orbit inclination (deg)	i	Normal
Payload	CCD Focus length (mm)	f_c	Normal
Multiple	Mission cycle (year)	T_{life}	Normal
Propulsion	Efficiency	η_t	Normal
	Input power (kW)	P_t	Normal
	Isp (s)	I_{sp}	Normal
Power	Solar energy-conversion efficiency	η_a	Normal
	Solar array energy-mass density (W h/kg)	γ_a	Normal
	Average discharge depth	DOD	Normal
Multiple	System mass margin	ε_m	Interval
	System power margin	ε_p	Interval

Problem Formulation

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- Reliability-based robust design optimization (RBRDO)

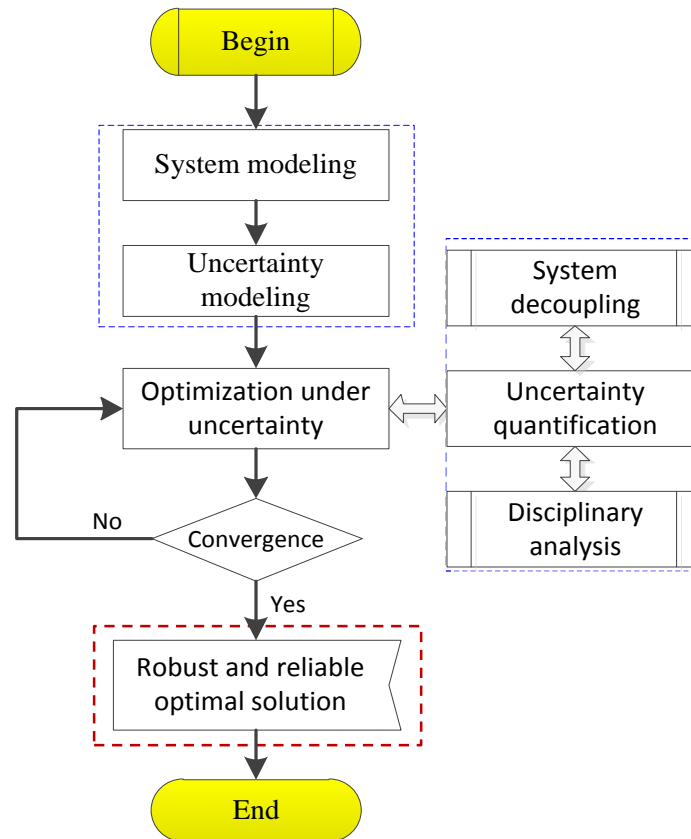
$$\left\{ \begin{array}{l} \text{find} \quad \mu_{\mathbf{x}} = [\mu_h \quad \mu_i \quad \mu_{f_c} \quad \mu_{T_{life}}] \\ \text{min} \quad \int f_C d\omega, \int f_M d\omega, \sqrt{\int f_C^2 d\omega - (\int f_C d\omega)^2} \\ \text{s.t.} \quad g_1 : \Pr\{d_s \leq 30\text{m}\} \geq 0.99 \\ \quad \quad g_2 : \Pr\{F_{str} > 1\} \geq 0.99 \\ \quad \quad g_3 : \Pr\{V_{sat} \leq 3U\} \geq 0.99 \\ \quad \quad g_4 : \Pr\{N_{Ba} \leq 10,000\} \geq 0.99 \\ \quad \quad 200\text{km} \leq \mu_h \leq 600\text{km}, 80^\circ \leq \mu_i \leq 90^\circ \\ \quad \quad 20\text{mm} \leq \mu_{f_c} \leq 200\text{mm}, 2a \leq \mu_{T_{life}} \leq 6a \end{array} \right.$$

$$f_C = C_{sat} / \left(D_r T_w \frac{365 L_T}{M_c} \right) \quad f_M = \sum M_{\text{sub},i}$$

Optimization Methodology

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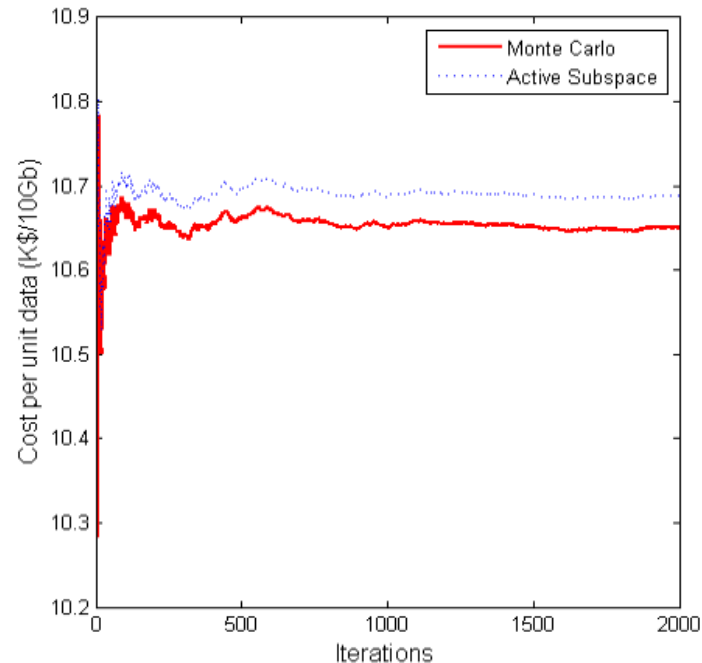
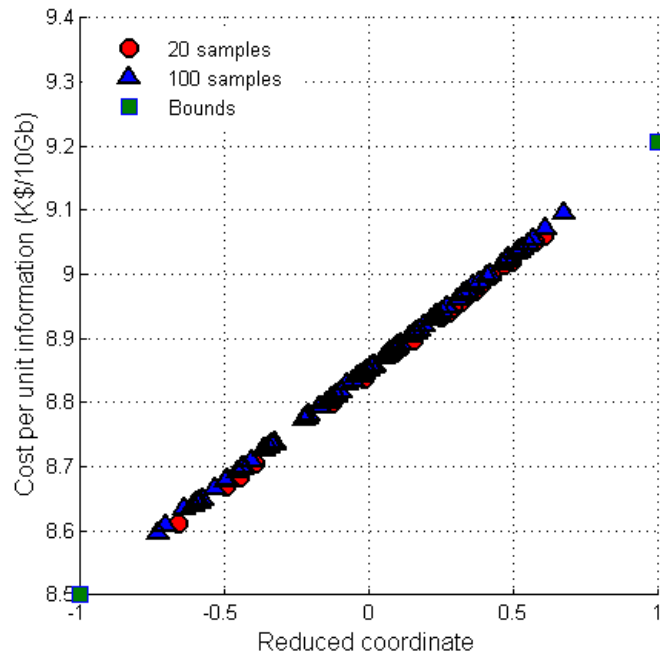
● Optimization workflow



Optimization Methodology

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- In-loop uncertainty quantification
 - Previous methods: Monte Carlo; polynomial chaos, compressed sensing...
 - Our method: identify a one-dimensional active subspace



Applied to 3U lunar CubeSat

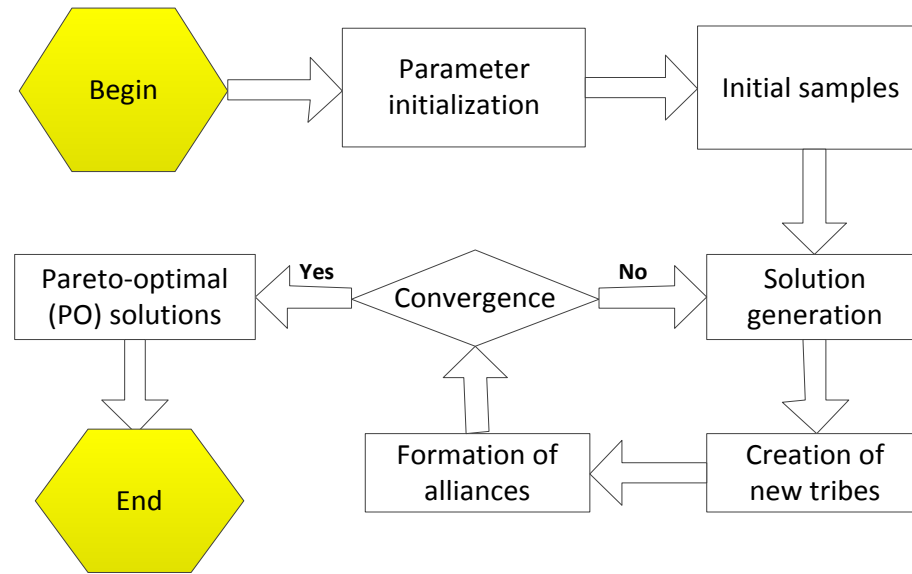


Optimization Methodology

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- Multi-objective solver
 - Previous algorithms: MOGA, NSGA-II, MOPS..
 - Our method:

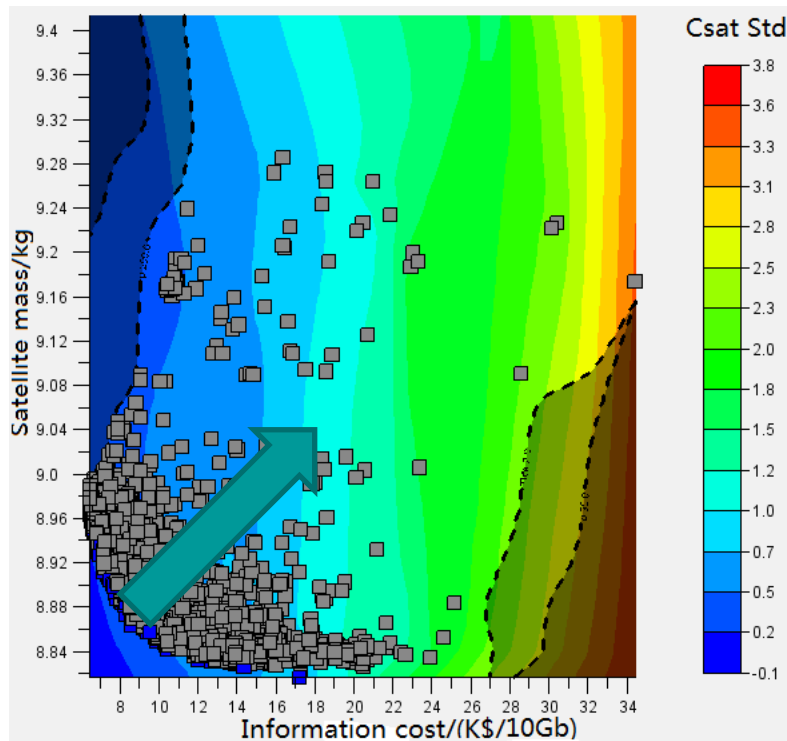
Multi-objective alliance algorithm (**MOAA**)



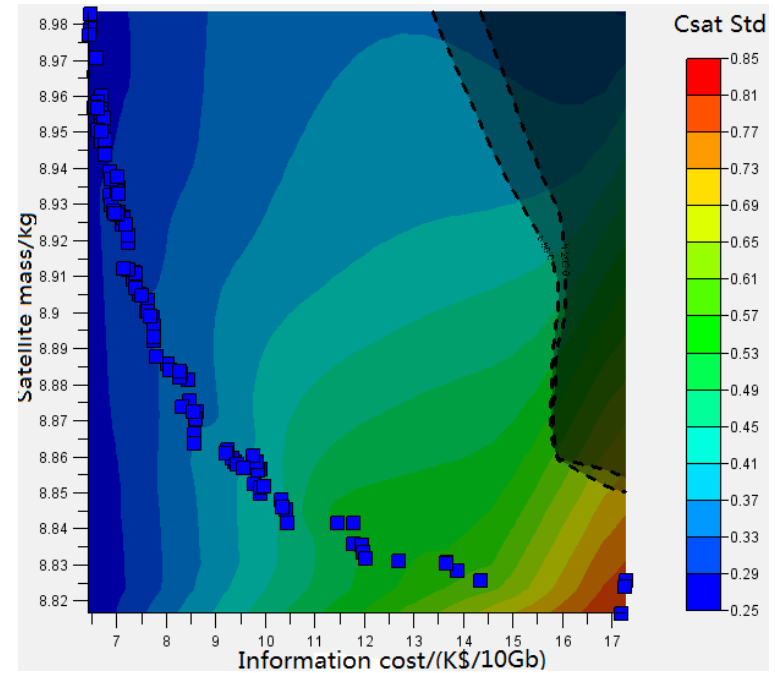
Results & Discussions

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● RBRDO solutions



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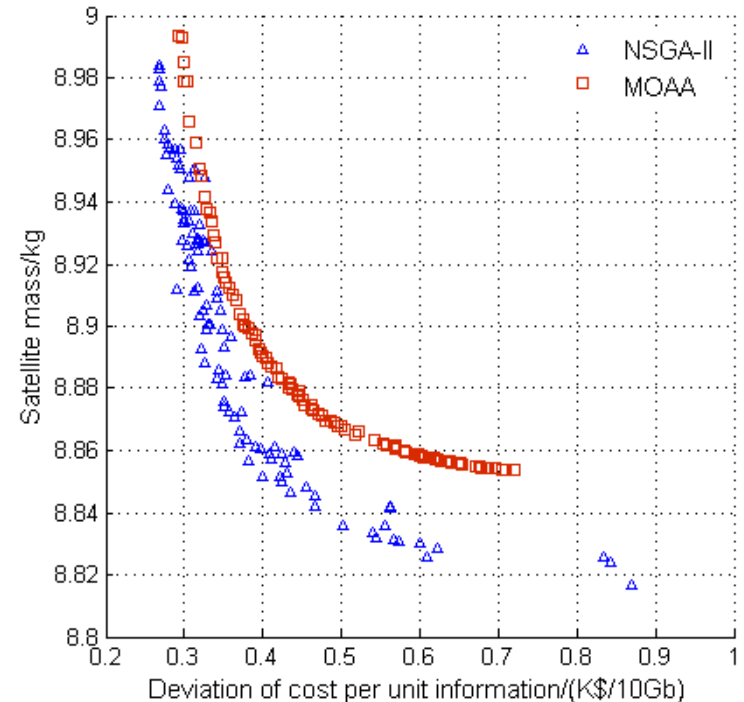
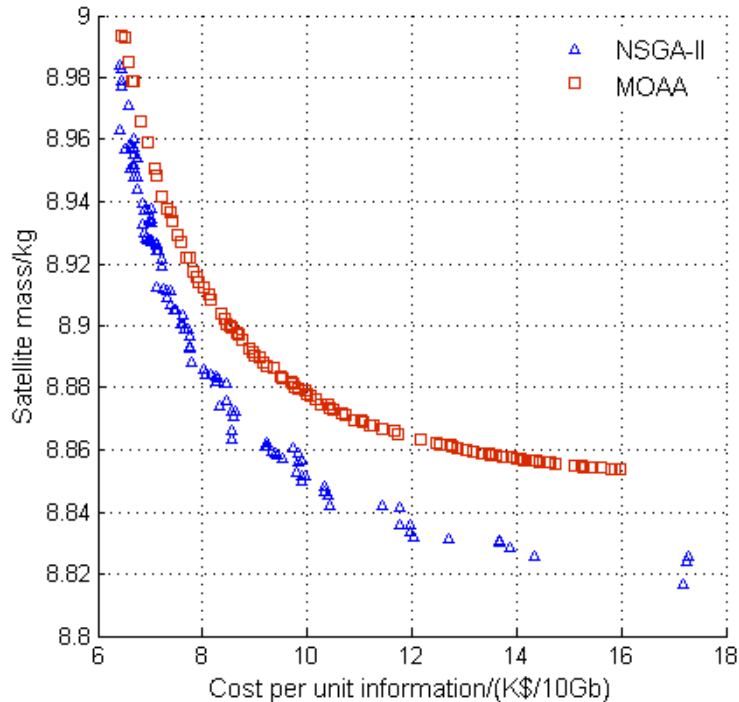


Pareto front

Results & Discussions

- Pareto comparison

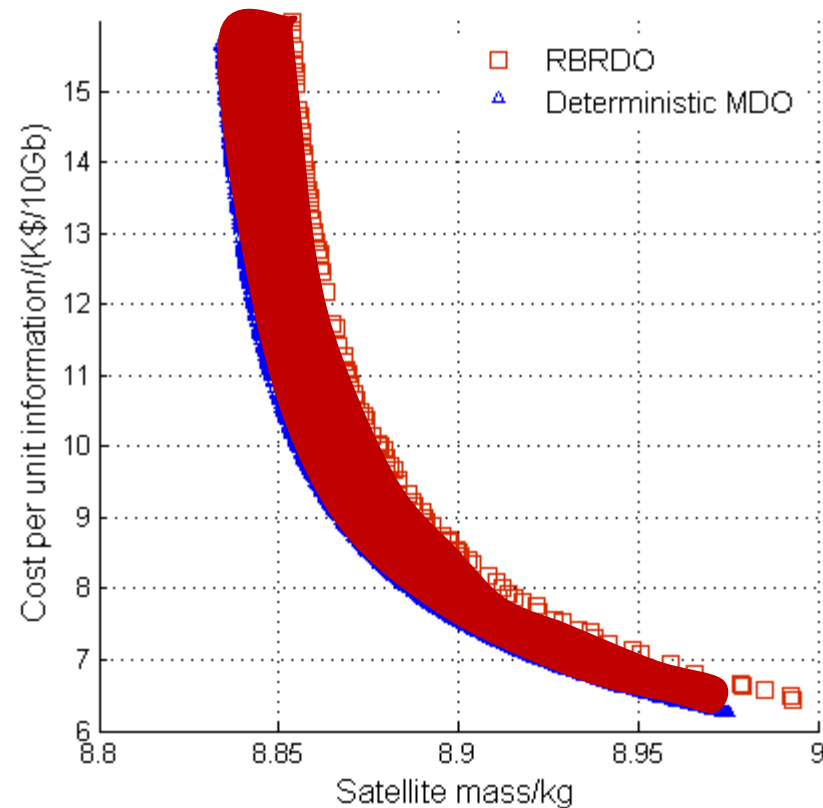
- MOAA vs. NSGA-II



Results & Discussions

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- Deterministic vs. Nondeterministic



Conclusions

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- Take home messages



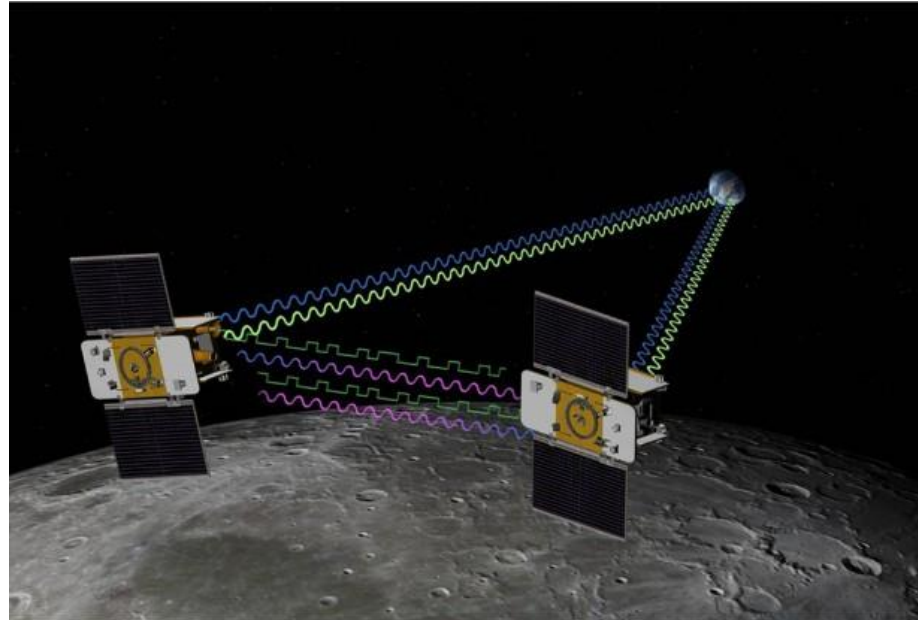
Conclusions

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- MOAA and active subspaces work.
- RBRDO worthwhile for lunar CubeSats.
- Reference for conceptual design and parameter control.
- Further perfected and demonstrated in near missions.



Thank You



CubeSat is revolutionizing aerospace science and engineering.